

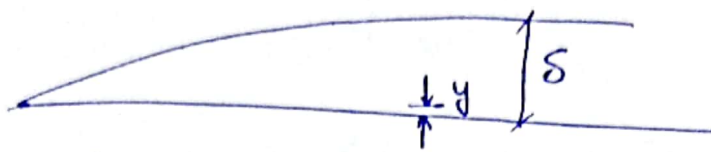
The law of the wall

- * It is one of the most famous empirically-determined relationship in turbulent flow near solid boundaries.
- * From measurements, for both internal and external flows, the streamwise velocity in the flow near the wall varies logarithmically with distance from surface. law of the wall
- * High Re turbulent boundary layers $\xrightarrow{\text{gives}}$ approximate description of the near-surface turbulence statistics
- * near the surface in turbulent boundary layer
 - The effect of the fluid's inertia & the pressure gradient are small.
 - statistics of the flow are established by two primary mechanisms :-
 - ① rate of transferred momentum to surface per unit area per unit time $\xrightarrow{\text{equal to}}$ local shear stress τ
 - ② molecular diffusion of momentum \longrightarrow plays an important role very close to surface.
 - The details of the eddies farther from the surface are of little importance to the near-wall flow statistics.
 - $\frac{y}{\delta}$ decreasing \longrightarrow improve the validity of

this approximate description.

δ is the boundary layer thickness

proof



- $\frac{\text{typical eddy size far from surface}}{\text{eddy size close to surface}} \uparrow \text{ as } \frac{y}{\delta} \downarrow$

- $\delta \uparrow \quad Re \uparrow$

at high Re a wide separation of scales appears

- τ varies near surface, although y is fairly slow.

→ τ_w : surface shear stress is used in dimensional analysis in place of local shear stress τ

- Turbulence behaves the same in gases and liquids → start with $\frac{\tau_w}{\rho}$ & $\nu = \frac{\mu}{\rho}$

- $\frac{\tau_w}{\rho} : \frac{m^2}{s^2}$

$\frac{\mu}{\rho} : \frac{m^2}{s}$

- length scale $\frac{\nu}{u_\tau}$ as $u_\tau \equiv \sqrt{\frac{\tau_w}{\rho}}$

as $u_\tau =$ friction velocity: velocity scale represent velocities close to solid boundary

$$\frac{\partial U}{\partial y} = \frac{U_\tau}{y} F\left(\frac{U_\tau y}{\nu}\right)$$

Kármán's constant

$F\left(\frac{U_\tau y}{\nu}\right)$: universal function $\rightarrow \frac{1}{K}$ as $\frac{U_\tau y}{\nu} \rightarrow \infty$

It approaches a constant value

means viscous effects cease to matter far from surface.

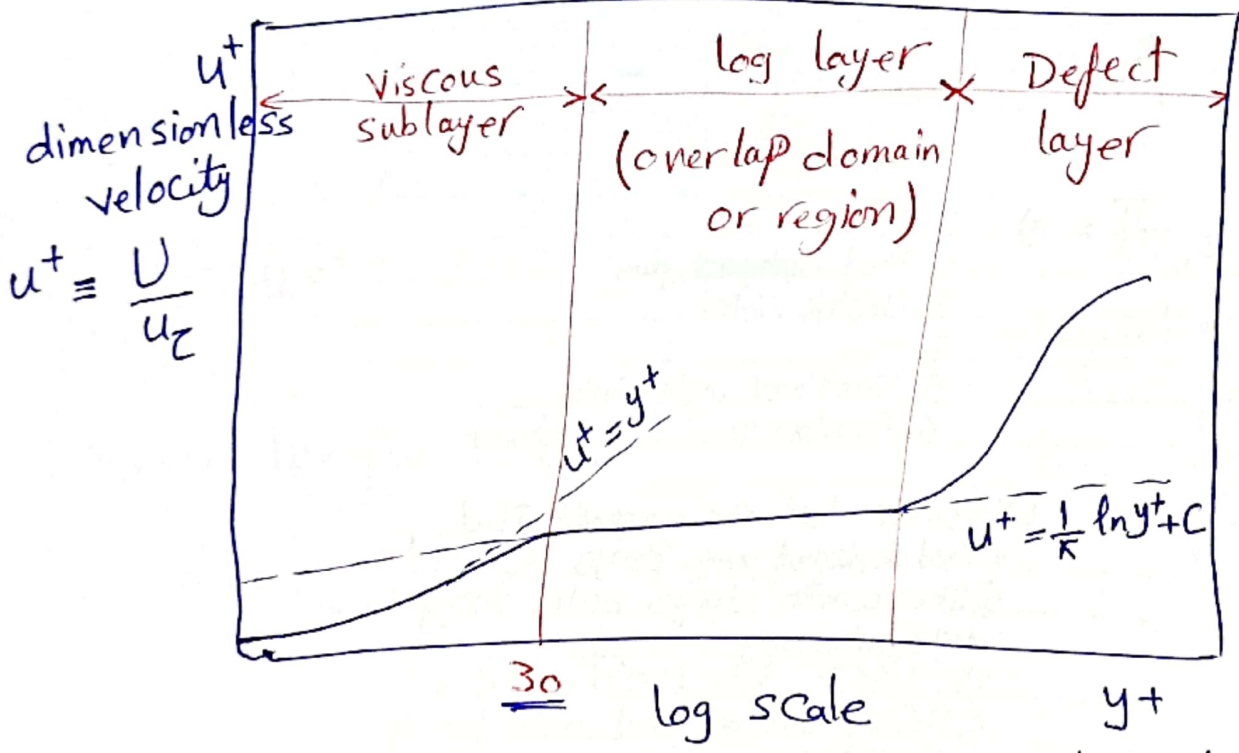
integrate over y

$K \approx 0.41$ for smooth surfaces

$$\frac{U}{U_\tau} = \frac{1}{K} \ln \frac{U_\tau y}{\nu} + C$$

$K \approx 0.41$ for smooth & rough surfaces

$$u^+ = \frac{1}{K} \ln y^+ + C$$



Definition of log layer

It is the portion of the boundary layer where sub layer and defect layer merge and the law of the wall accurately represents the velocity

* log layer is not a distinct layer.

It is an overlap region between the inner and outer parts of the boundary layer.

* The velocity in the viscous sublayer

$$U = u_{\tau} f(y^+) \xrightarrow{\text{law of the wall}}$$

dimensionless function

* In the defect layer, numerous experiment found that velocity data correlate reasonably well with the so-called velocity-defect law (Clouser defect law)

$$U = U_e - u_{\tau} g(\gamma)$$

dimensionless function

velocity at the boundary-layer edge

as $\gamma = \frac{y}{\Delta}$

↑

thickness characteristic of the outer portion of the boundary layer

* inner length scale $\frac{\nu}{u_{\tau}}$

outer length scale Δ

* If a wide separation of scales exists

$$\frac{\nu}{u_{\tau}} \ll \Delta \qquad \frac{m^2/s}{m/s} = m$$

then an overlap domain exists such that

$$u_{\tau} f(y^+) = U_e - u_{\tau} g(\gamma) \quad \text{for } y^+ \gg 1 \text{ \& } \gamma \ll 1$$

differentiate with respect to y

$$\frac{u_\tau^2}{\nu} f'(y^+) = -\frac{u_\tau}{\Delta} g'(\gamma)$$

$$\begin{aligned} * \frac{y}{u_\tau} \\ y^+ = \frac{u_\tau y}{\nu} \neq \\ \gamma = \frac{y}{\Delta} \end{aligned}$$

$$y^+ f'(y^+) = -\gamma g'(\gamma)$$

a wide separation of scales means y^+ and γ are independent variables

$$y^+ f'(y^+) = \text{const} = \frac{1}{K}$$

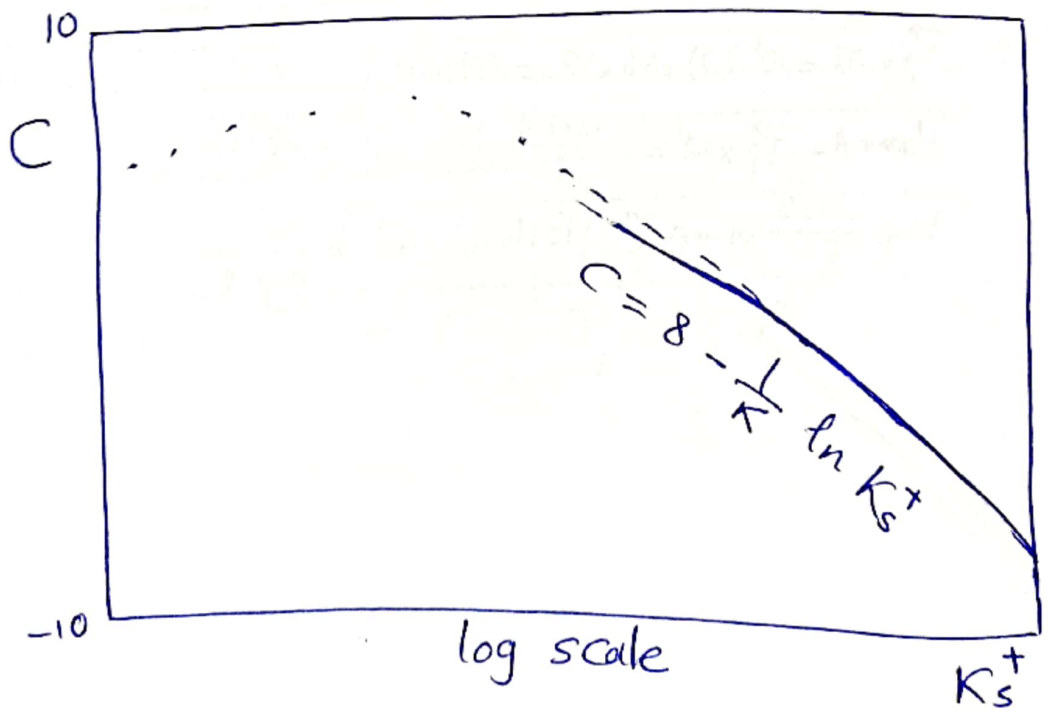
$$F(y^+) = \frac{1}{K} \ln y^+ + C$$

$C \approx 5$ for perfectly-smooth surfaces

* For surfaces with roughness elements of average height K_s

dimensionless roughness $K_s^+ \equiv \frac{u_\tau K_s}{\nu}$

for a large roughness height $C \rightarrow 8 - \frac{1}{K} \ln K_s^+ \quad K_s^+ \gg 1$



as $K_s \uparrow \quad C \downarrow$

$$\frac{U}{u_\tau} = \frac{1}{\kappa} \ln \frac{u_\tau y}{\nu} + C$$

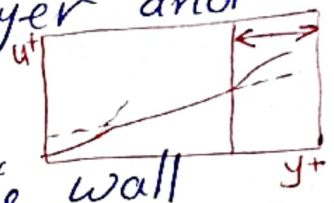
sub. with C

$$\frac{U}{u_\tau} = \frac{1}{\kappa} \ln \left(\frac{y}{\kappa_s} \right) + 8$$

for completely-rough wall

* The absence of viscosity in this equation because the surface "shear stress" is due to pressure drag on the roughness elements.

* Defect layer lies between log layer and the edge of the boundary layer.



the velocity follows the law of the wall as $\frac{y}{\delta} \rightarrow 0$

$$U^+ = \frac{1}{\kappa} \ln y^+ + C + \frac{2\Pi}{\kappa} \sin^2 \left(\frac{\pi}{2} \frac{y}{\delta} \right)$$

coles' wake-strength parameter ≈ 0.6 from measurements

Composite law of the wall and law of the wake profile

boundary layer thickness

* The velocity in the defect layer varies like the equilibrium parameter $\rightarrow \beta_T \equiv \left(\frac{\delta^*}{\tau_w} \frac{dP}{dx} \right) \rightarrow$ mean pressure displacement thickness

* equilibrium turbulent boundary layer boundary layer at which β_T is constant

$$\Pi = 0.6 + 0.51 \beta_T - 0.01 \beta_T^2$$