



College of Engineering & Technology

Department: Mechanical Engineering
 Lecturer: Dr. Rola Afify
 Course Code: ME356

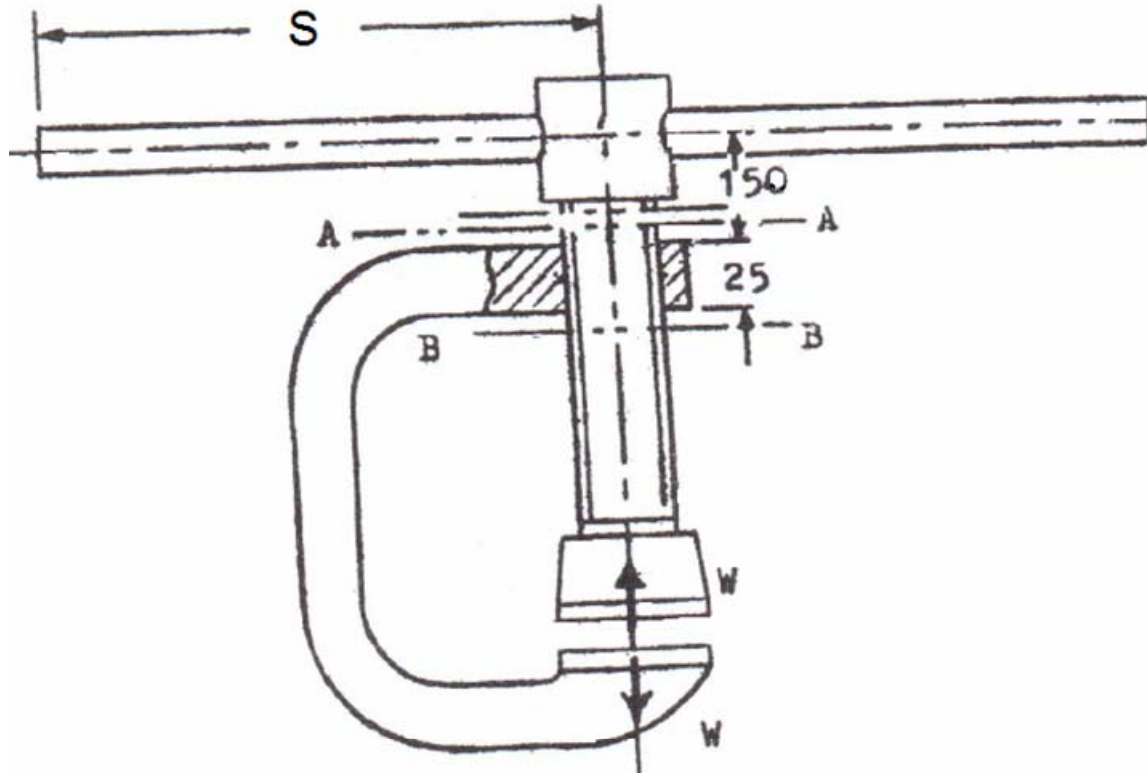
Marks: 20
 Time: 11.00 - 12.00
 Date: 16/12/2015

20

Name: **Model Answer**

R.N.: _____

Answer the following question:



The 70 mm double thread screw of a 10 kN shop press, shown in Figure, has an iso-trapezoidal thread. The operator's force may be taken 180 N for each hand. The mean diameter of collar is 60 mm.

You may use this

$$T = W \frac{dm}{2} \left[\frac{\pi \mu dm \sec \alpha + L}{\pi dm - \mu L \sec \alpha} \right] + \frac{\mu_c W dm_c}{2}$$

Determine:

$d_o = 70 \text{ mm}$ double thread $L = 2P$
 $W = 10 \text{ kN} = 10^4 \text{ Newton}$
 iso-trapezoidal $2\alpha = 3^\circ$ $\therefore \alpha = 1.5^\circ$
 $F_{\text{handle}} = 180 \text{ Newton}$ $d_{mc} = 60 \text{ mm}$

- a) The length S , assuming that the coefficient of friction is 0.12 in the threads and 0.125 at the collar. The inner diameter is 58 mm. The pitch is 12 mm.

Determine :-

a) $S = ??$

$$\mu = 0.12 \quad , \quad \mu_c = 0.125$$

$$d_i = 58 \text{ mm} \quad , \quad P = 12 \text{ mm}$$

Soln $d_m = \frac{d_i + d_o}{2} = \frac{58 + 70}{2} = 64 \text{ mm}$

$$L = 2P = 2 * 12 = 24 \text{ mm}$$

$$T = W \frac{d_m}{2} \left[\frac{\pi \mu d_m \sec \alpha + L}{\pi d_m - \mu L \sec \alpha} \right] + \frac{\mu_c W d_{mc}}{2}$$

$$= 10^4 * \frac{64}{2} * \left[\frac{\pi * 0.12 * 64 \sec 15 + 24}{\pi * 64 - 0.12 * 24 \sec 15} \right] + \frac{0.125 * 10^4 * 60}{2}$$

$$T = 116625.1575 \text{ N}\cdot\text{mm}$$

$$T = F_{\text{handle}} * 2S = 360 S$$

$$\therefore S = 323.96 \text{ mm} \approx 324 \text{ mm}$$

- b) The efficiency of the press.

b) $\eta = ??$

Soln $T_0 = \frac{WL}{2\pi} = \frac{10^4 * 24}{2\pi} = 38197.2 \text{ N}\cdot\text{mm}$

$$\eta = \frac{T_0}{T} = \frac{38197.2}{116625.16} = 0.3275 \approx 0.33$$

- c) Is the screw self-locking? Explain.

Soln

$$\begin{array}{l} \pi \mu d_m \sec \alpha > L \\ \pi * 0.12 * 64 \sec 15 > 24 \\ 24.97855 > 24 \end{array}$$

self-locking

- d) The maximum normal and shear Stresses in the screw.

d) $\sigma_{\text{max}} , \tau_{\text{max}} = ??$

sec A-A $\sigma_b = 0 \quad \tau = \frac{Tr}{J}$

$$\tau = \frac{T r}{J} = \frac{116625.16 * \frac{58}{2}}{\frac{\pi}{32} (58)^4} = 3 \text{ MPa}$$

$$\sigma_{\max} = \frac{\sigma}{2} + \sqrt{\left(\frac{\sigma}{2}\right)^2 + \tau^2} = 0 + \sqrt{0^2 + 3^2} = 3 \text{ MPa}$$

$$\tau_{\max} = \sqrt{\left(\frac{\sigma}{2}\right)^2 + \tau^2} = \sqrt{0^2 + 3^2} = 3 \text{ MPa}$$

sec B-B

$$\sigma_c = \frac{F}{A} = \frac{W}{\frac{\pi}{4} d_i^2} = \frac{10^4 * 4}{\pi (58)^2} = 3.785 \text{ MPa}$$

$$T_c = \frac{\mu W d m c}{2} = \frac{0.125 * 10^4 * 60}{2} = 37500 \text{ N}\cdot\text{mm}$$

$$\tau = \frac{T_c r}{J} = \frac{37500 * \frac{58}{2}}{\frac{\pi}{32} (58)^4} = 0.979 \text{ MPa}$$

$$\begin{aligned} \sigma_{\max} &= \frac{\sigma}{2} + \sqrt{\left(\frac{\sigma}{2}\right)^2 + \tau^2} \\ &= \frac{3.785}{2} + \sqrt{\left(\frac{3.785}{2}\right)^2 + (0.979)^2} = 4.023 \text{ MPa} \end{aligned}$$

$$\begin{aligned} \tau_{\max} &= \sqrt{\left(\frac{\sigma}{2}\right)^2 + \tau^2} \\ &= \sqrt{\left(\frac{3.785}{2}\right)^2 + (0.979)^2} = 2.13 \text{ MPa} \end{aligned}$$

$$\sigma_{\max} = 4.023 \text{ MPa sec B-B} \quad \& \quad \tau_{\max} = 3 \text{ MPa sec A-A}$$

e) The shear stress on the screw and nut threads.

$$e) \tau_{\text{screw}} = ?? \quad \& \quad \tau_{\text{nut}} = ?? \quad \text{shear stress on threads}$$

$$\begin{aligned} \text{soln} \quad \tau_{\text{screw}} &= \frac{2W}{\pi d_i H} \quad \text{from drawing } H = 25 \text{ mm} \\ &= \frac{2 * 10^4}{\pi * 58 * 25} = 4.39 \text{ MPa} \end{aligned}$$

$$\tau_{\text{nut}} = \frac{2W}{\pi d_o H} = \frac{2 * 10^4}{\pi * 70 * 25} = 3.64 \text{ MPa}$$

f) The bearing stress in the threads.

$$f) \sigma_{\text{br}} = ??$$

$$\text{soln} \quad \sigma_{\text{br}} = \frac{2W}{\pi d_m H} = \frac{2 * 10^4}{\pi * 64 * 25} = 3.98 \text{ MPa}$$