



COLLEGE OF ENGINEERING & TECHNOLOGY

Department : Mechanical Engineering

Lecturer : Staff

Course : Machine design

Course Code: ME 454

Date : 08/ 06 / 2016

Marks: 40

Time: 12.00:14.00

FINAL EXAMINATION PAPER

ANSWER 4 QUESTIONS ONLY

QUESTION (1) [10 MARKS]

Fig. 1 shows a schematic drawing of a countershaft that supports two V-belt pulleys. The belt tension on the loose side of pulley A is 20 percent of the tension on the tight side. The shaft material has an ultimate strength of 500 MPa and yield strength of 310 MPa. Determine:

- The necessary shaft diameter using $k_b = 1.5$ and $k_t = 1$.
- Compute the components of the force with which the bearings at O and E push against the shaft.

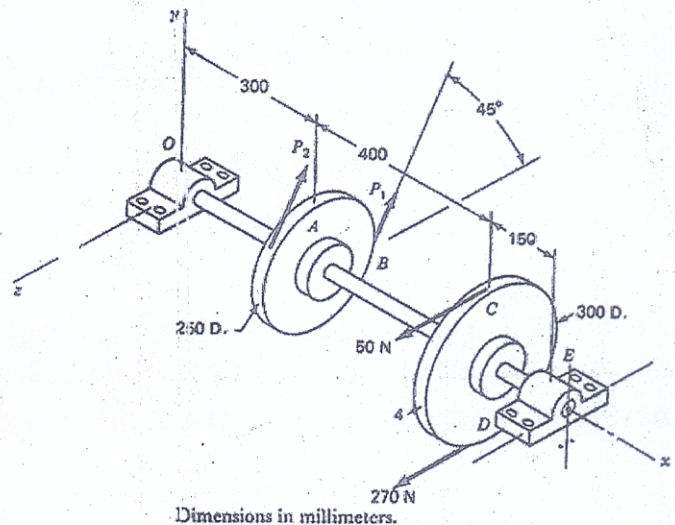


Figure (1)

QUESTION (2) [10 MARKS]

A load "F" of 10 kN is suspended from a plate "a" held by bolts 1, 2 and 3. The thickness of the plate $h = 14$ mm, $L_1 = 250$ mm, $L_2 = L_3 = 100$ mm. The bolts are made of steel, $S_y = 400$ MPa.

Determine:

- The bolt size with a safety factor of 1.7.
- The stresses in bolts 1 and 3 if bolt 2 is taken out, see Fig. 2.

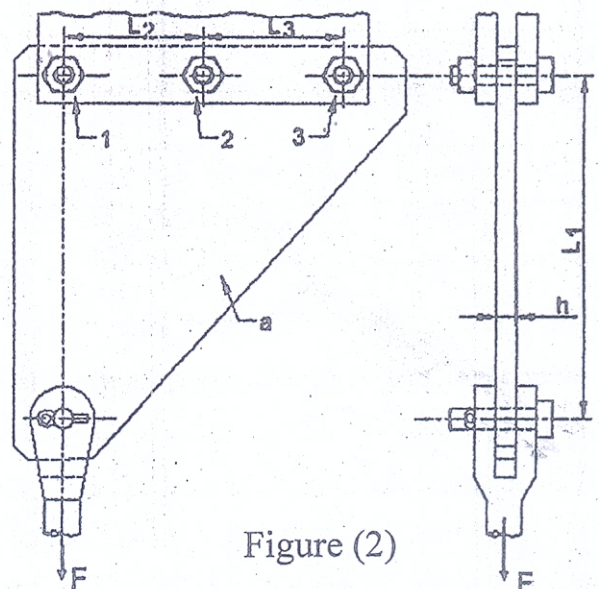


Figure (2)

QUESTION (3) [10 MARKS]

A hollow circular shaft of 200 mm outside diameter and 175 mm inside diameter is fitted with a wringing fit to the hole in the boss of a forged flange. The two are then secured by fillet welding as shown in Fig.3. The welded flange is to be bolted to a smooth vertical face, not shown. Determine the weld size if the allowable shear stress for the weld is 100 MPa.

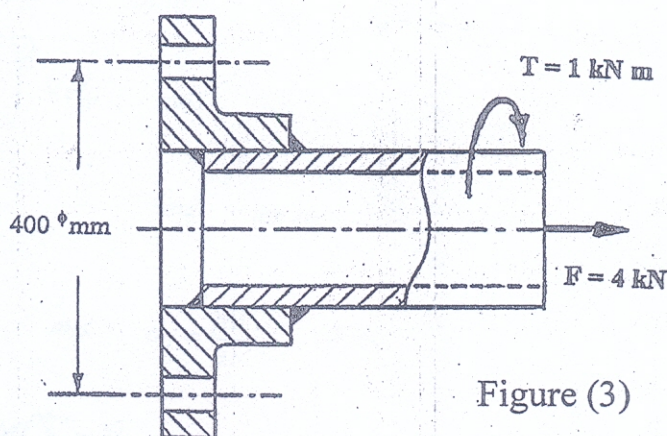


Figure (3)

QUESTION (4) [10 MARKS]

A square power transmission screw of a screw press is required to transmit maximum load of 60 kN. The screw outside diameter is 70 mm with a pitch of 12 mm, the coefficient of friction is 0.12 in the threads and 0.125 in the thrust collar and the thrust collar diameter is 60 mm. Determine:

- The torque required to move the load.
- The efficiency of the threads.
- The maximum normal and shear stresses in the screw.
- The bearing pressure in the threads if the height of nut is 240 mm.

QUESTION (5) [10 MARKS]

- Determine the recommended belt velocity for a V-belt drive so that the power transmitted is maximum.
- The drive from a motor to a centrifugal pump consists of three size C V-belt. The motor pulley has a 240 mm pitch diameter and the pump pulley has a 400 mm pitch diameter. The motor runs at 1200 rpm. The belt angle is 40° . What power can be transmitted if the centre distance is 1 m? Belt cross sectional area equal 230 mm^2 , belt density is 1150 kg/m^3 , coefficient of friction is 0.13 and the allowable tensile stress is 2 MPa.

GOOD LUCK

Machine Design (ME 454)

Direct normal stress : $\sigma_d = \frac{F}{A}$ Direct shear stress : $\tau_d = \frac{F}{A_s}$

Bending stress : $\sigma_b = \frac{M y}{I}$ Torsion stress : $\tau = \frac{T r}{J}$

Stresses on inclined planes :

$$\sigma_\theta = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta \quad \text{and} \quad \tau_\theta = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad \text{and} \quad \tan 2\theta_p = \frac{\tau_{xy}}{(\sigma_x - \sigma_y)/2}$$

$$\tau_{\max/\min} = \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad \text{and} \quad \tan 2\theta_s = \frac{-(\sigma_x - \sigma_y)/2}{\tau_{xy}}$$

Pressure vessels :

$$\sigma_1 = \frac{p d}{2t} \quad \text{and} \quad \sigma_2 = \frac{p d}{4t}$$

Bolted connections :

Tensile load due turning : $f = M / \sum n_i r_i^2$ Secondary shear : $s = T / \sum r_i^2$

Pre loading : $\delta = \frac{F l}{A E}$, $F_b = \left(\frac{k_b}{k_b + k_m}\right) F_e + F_i$, $F_m = \left(\frac{k_m}{k_b + k_m}\right) F_e - F_i$

$$F_p = A_t S_p , \quad S_p = 0.85 S_y , \quad F_i = \begin{cases} 0.75 F_p \\ 0.90 F_p \end{cases} , \quad F_i \geq (1 - C) F_e \text{ where } C = \frac{k_b}{k_b + k_m}$$

Welded joints :

Bending stress $\sigma = \frac{M c}{0.707 h I_u}$, Secondary shear stress $\tau_s = \frac{T r}{0.707 h J_u}$

Power screws :

$$\begin{aligned} \text{lifting} &= \frac{F d_m}{2} \left(\frac{\pi \mu d_m \sec \alpha \pm l}{\pi d_m \mp \mu l \sec \alpha} \right) + \frac{F \mu_c d_c}{2} , & e &= \frac{F l}{2 \pi T} , \text{ Self locking : } \mu > \tan \lambda \cos \alpha \\ \text{lowering} & \end{aligned}$$

Belt drive :

Power = $(F_1 - F_2) V$, Open drive : $\theta_{1,2} = \pi \mp 2 \sin^{-1} \left(\frac{d_2 - d_1}{2C} \right)$

$$\frac{\text{Power}}{m^2} = (\sigma_{all} - \omega V^2) V \left(\frac{e^{f\theta} - 1}{e^{f\theta} - 1} \right) , \quad \frac{F_1 - F_c}{F_2 - F_c} = e^{f\theta} , \quad F_c = \text{mass per unit length} \times V^2$$

Shaft design;

$$d_o^3 = \frac{16}{\pi \tau_{all} (1 - c^4)} \sqrt{\left(k_b M_b + \frac{\alpha F_a d_c (1 + c^2)}{8} \right)^2 + (k_t M_t)^2}$$



$$A = 1.414 \pi r^2$$

$$J_u = 2 \pi r^3$$

$$J_u = \pi r^3$$