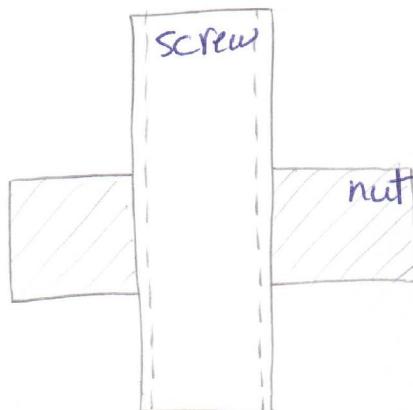
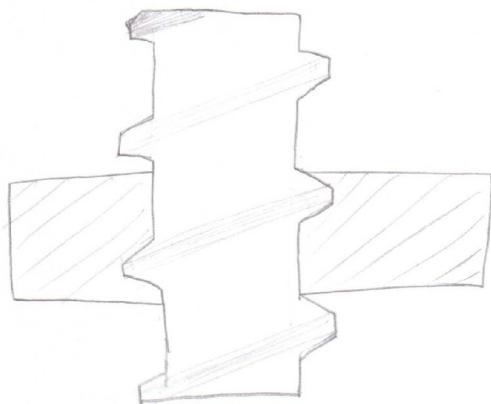
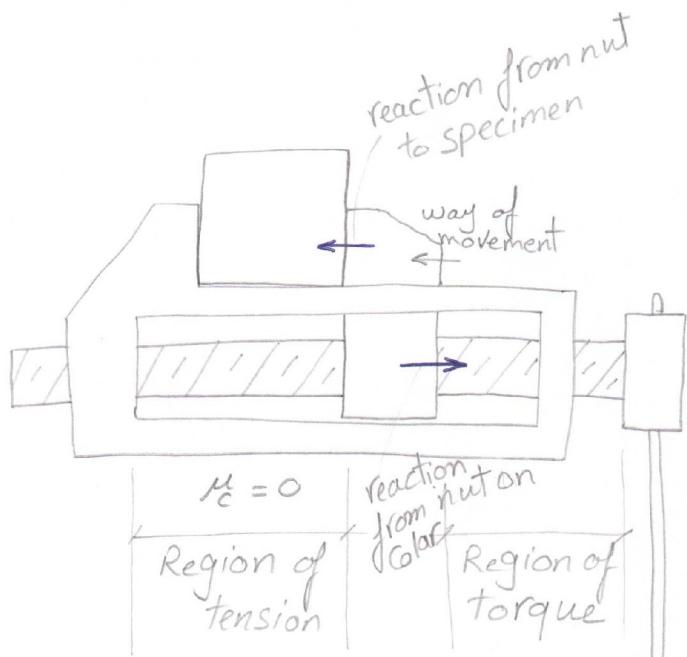
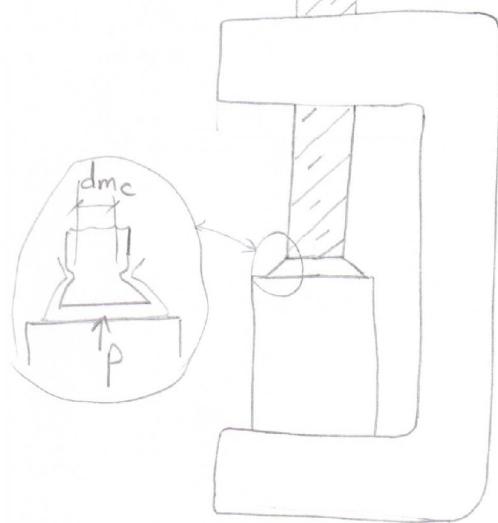
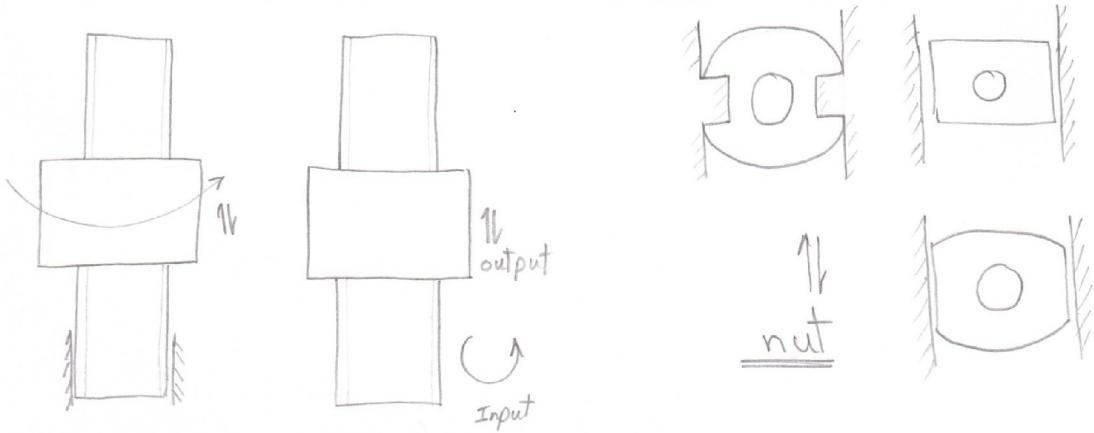
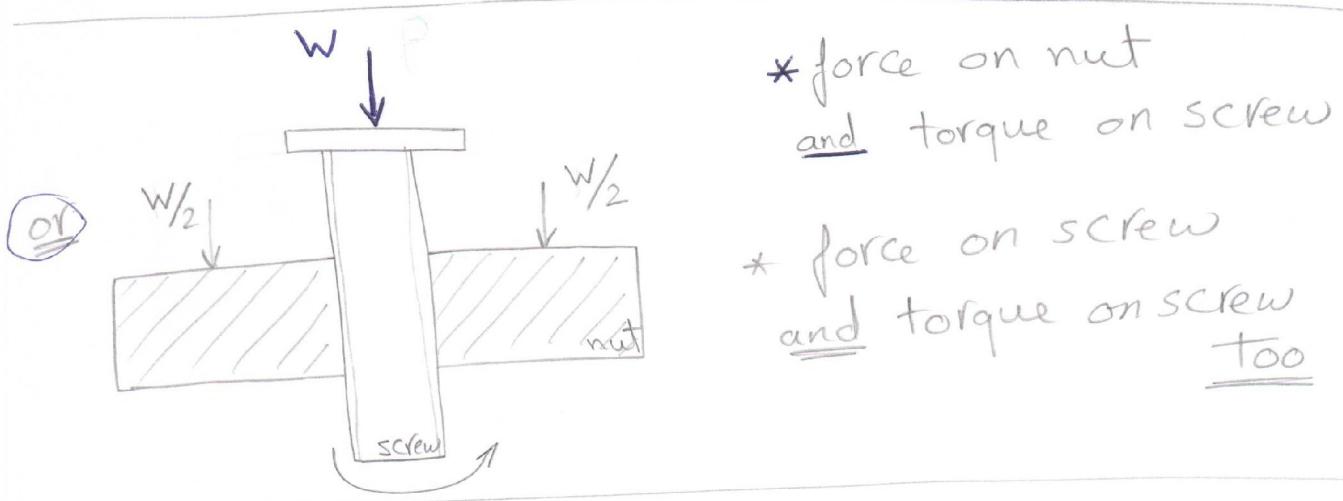
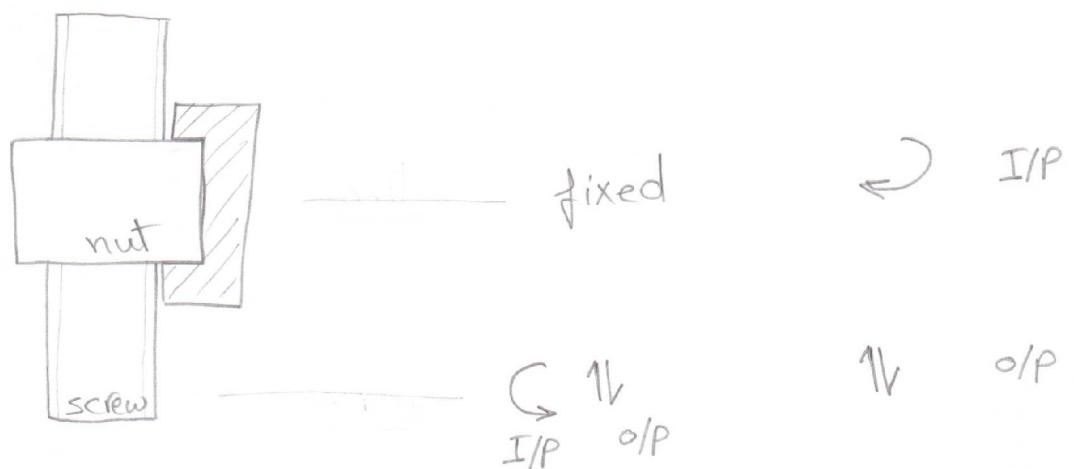


power screw

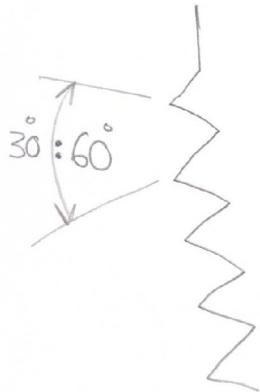


* relative motion between screw and nut



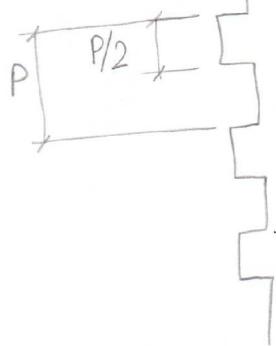


Threads
*triangular



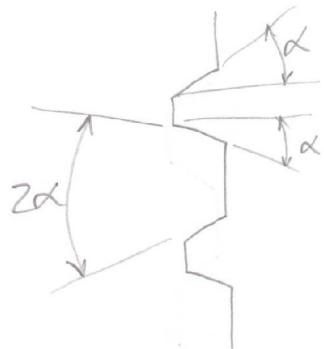
more frictional
less efficiency

* Rectangular
(square)



$$P = d_o - d_i$$

* trapezoidal



* iso-trapezoidal
 $2\alpha = 30^\circ$

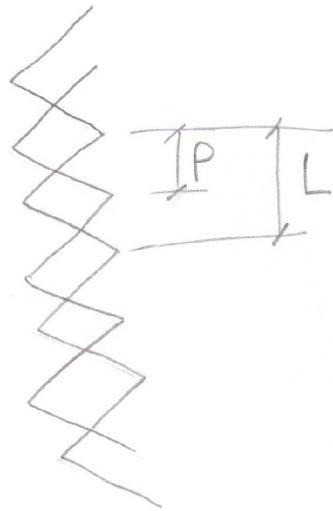
single thread $n=1$

$n=2$
double & more

$$L = n P$$



(L) depends
on no. of threads



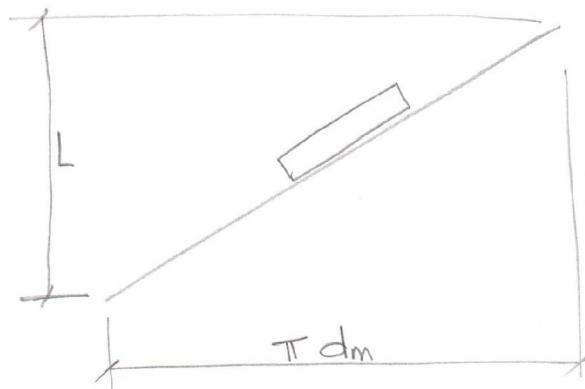
$$\text{lead } (L) = P$$

$$L = 2P$$

- * double thread has more efficiency in moving than single thread for same no. of teeth for one thread.

$$d_m = \frac{d_o + d_i}{2}$$

- if a point on ^{a single} thread of screw moves one cycle it moves a distance equal to a pitch



- * High friction between fasteners and members used for high hold.
- * Low friction in power screw is needed to transmit motion (from rotational motion to linear motion).

Force Analysis *for lifting & lowering

force

$$F = W \left[\frac{\pi \mu d_m + L}{\pi d_m - \mu L} \right]$$

torque

$$T = W \cdot \frac{d_m}{2} \left[\frac{\pi \mu d_m \pm L}{\pi d_m \mp \mu L} \right]$$

lifting
lowering

* ↑ lifting → opposite direction to load ↓

↓ lowering → indirection ~ of ~ ↓

* d_m : mean diameter L : lead μ : coefficient of friction

W : exerted force \Rightarrow square thread

* $L < \pi d_m \mu$ self locking

$L > \pi d_m \mu$ not self locking

* IF $\mu = 0$ (no friction case) $T_o = \frac{WL}{2\pi}$

* Efficiency $\gamma = \frac{T_o}{T}$

* for trapezoidal thread with an axial load

color betw
rotating and
stationary
members

$$T = \frac{W d_m}{2} \left[\frac{\pi \mu d_m \sec \alpha + L}{\pi d_m - \mu L \sec \alpha} \right] + T_c$$

α : trapezoidal angle

T_c : color frictional torque

$$T_c = \frac{\mu c W d_m c}{2}$$

bearing is \rightarrow \rightarrow \rightarrow

$$\therefore T_c = 0$$

* stresses in power screw

① screw

Torsion

$$\tau = \frac{\text{sec A-A}}{J}$$

$$C = \frac{T * r}{J}$$

bending

$$\sigma_b = \frac{M y}{I}$$

$$M = F_{\text{handle}} * l$$

$$\sigma_{\max} = \sqrt{\left(\frac{\sigma_b}{2}\right)^2 + C^2} = \frac{0.5 S_y}{F.S.}$$

sec B-B

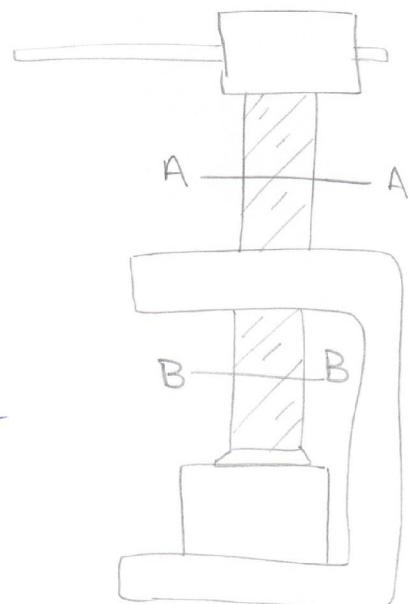
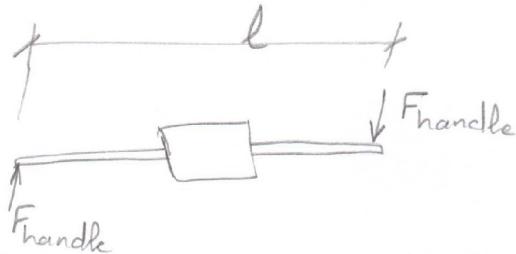
Compression

$$\sigma_c = \frac{W}{A} = \frac{W}{\frac{\pi}{4} d_i^2}$$

check for buckling $F_{cr} = \leftarrow$

torsion

$$\tau = \frac{T_c * r}{J}$$



② thread

$$\text{Load/tooth} = \frac{W}{\text{no. of teeth (N)}}$$

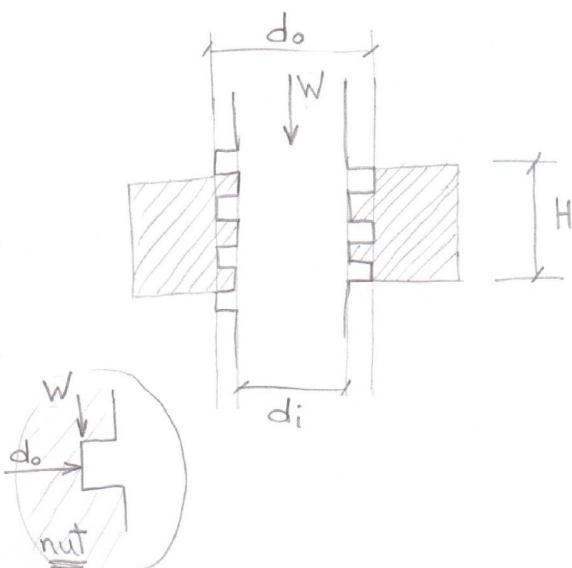
$$H = \text{height of nut} = N * P$$

$$\text{Area of shear stress} = \pi d_i * \frac{P}{2}$$

$$\begin{aligned} \tau_{\text{scREW}} &= \frac{\text{Load/tooth}}{\text{Area}} = \frac{W/N}{\pi d_i * \frac{P}{2}} \\ &= \frac{2W}{\pi d_i H} \end{aligned}$$

$$\begin{aligned} \tau_{\text{nut}} &= \frac{2W}{\pi d_o H} \end{aligned}$$

→ screw



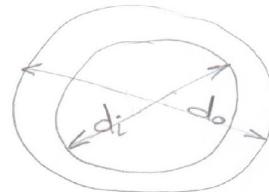
bearing

$$\sigma_{br} = \frac{\text{load / tooth}}{\text{projected area}} = \frac{W/N}{\frac{\pi}{4} (d_o^2 - d_i^2)}$$

$$= \frac{W/N}{\frac{\pi}{4} (d_o - d_i) (d_o + d_i)}$$

$$= \frac{W}{\frac{\pi}{4} * z dm * P * N}$$

$$\sigma_{br} = \frac{z W}{\pi dm H}$$



$$d_o + d_i = 2 dm$$

$$d_o - d_i = P$$