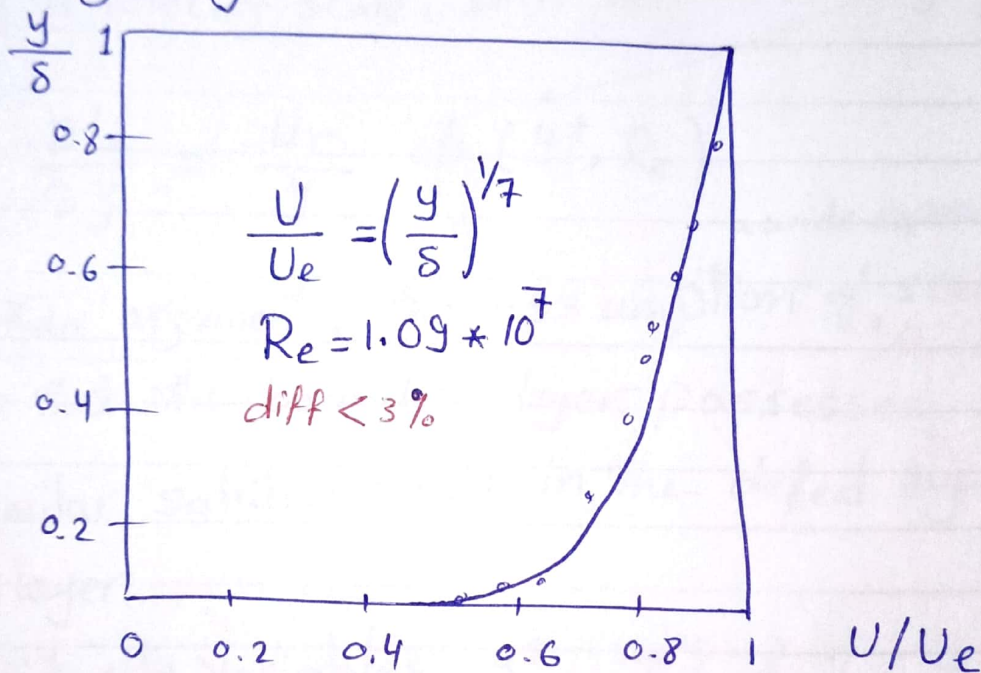


power laws

$$\frac{U}{U_e} = \left(\frac{y}{\delta}\right)^{1/n} \rightarrow \text{integer between 6 and 8}$$

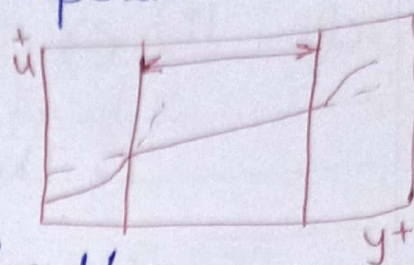
- * Power-law relationship is an approximation for turbulent boundary layer profiles.
- * Prandtl suggested $n=7$. this yields a good approximation at high Re for flat-plate boundary layer.



- * Barenblatt and others have challenged the validity of the law of the wall
 - a power-law variation of the velocity in the inner layer better correlates pipe-flow measurements and represents a more realistic description in a boundary layer.
 - Their critical assumption is the existence of a wide separation of scales (large $\frac{\delta}{(2l/u\tau)}$)

- They maintain that the turbulence in the overlap region is Re dependent.

- IF this ^{is} true



the law of the wall will be replaced by

$$U = u_\tau \tilde{f}(y^+, Re)$$

defect law will be replaced by $U = U_e - u_0 \tilde{g}(\eta, Re)$

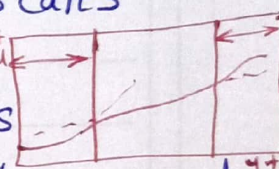
u_0 is a velocity scale. It is not necessarily equal to u_τ

$$\frac{\partial U}{\partial y} = \frac{u_\tau}{y} \Phi(y^+, Re)$$

a wide separation of

* In Millikan argument, the assumption of $1/s$ scales

implies that the boundary layer possesses self-similar solutions both in the defect layer and the sublayer.



- similarity variables $y^+ = \frac{u_\tau y}{\nu}$ & $\eta = \frac{y}{\Delta}$ exists in each region.

- the assumption that y^+ & η are distinct variables (described as complete similarity in the overlap region)

[by contrast, Barenblatt hypothesis corresponds to incomplete similarity]

* Incomplete similarity

$y^+ \rightarrow \infty$ $\Phi(y^+, Re)$ not necessarily approach a constant value even if $Re \rightarrow \infty$

(3)

$$\Phi(y^+, Re) = A(y^+)^{\alpha} \quad \text{for large } y^+$$

← Coefficient
fn of Re
← exponent
fn of Re

* Barenblatt, chorin and Prostopkishin assumed
 [incomplete similarity in y^+ and no similarity in Re]

- Combine the previous two equations

$$\frac{\partial U^+}{\partial y^+} = A(y^+)^{\alpha-1}$$

integrate ↙

$$U^+ = \frac{A}{\alpha} (y^+)^{\alpha}$$

- from experimental data for pipe flow

$$A = 0.577 \ln Re + 2.5 \quad \& \quad \alpha = \frac{1.5}{\ln Re}$$

Re based on average vel. and pipe diameter

* Zagarola, Perry and smits Considered more recent experiment with a much wider range of Re

- They concluded that classical law of the wall provides closer correlation with measurements than the power law & they recommend larger value of K of 0.44

- or use $A = 0.7053 \ln Re + 0.3055$ &

$$\alpha = \frac{1.085}{\ln Re} + \frac{6.532}{(\ln Re)^2} \quad \& \text{ still law of the wall is better}$$