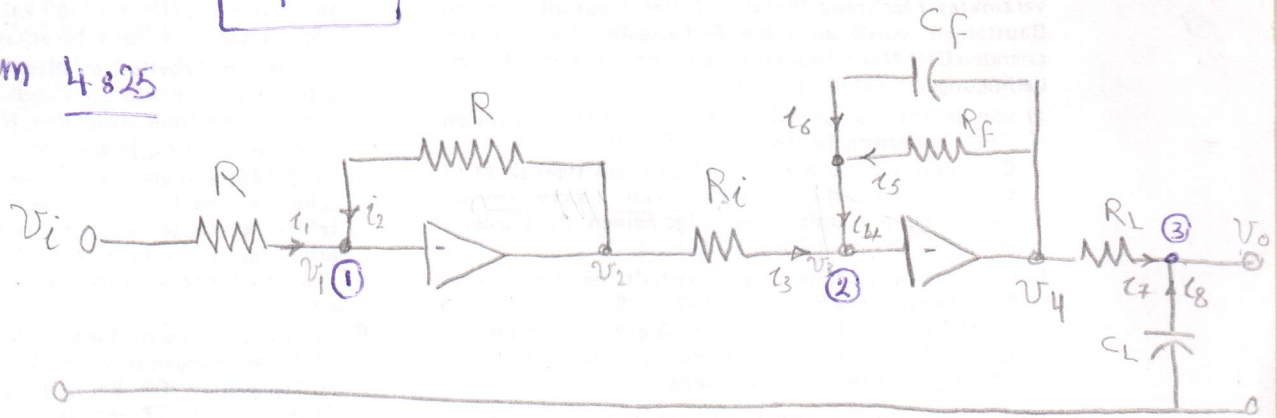


The op-amp equation:

$$V_+ \cong V_-$$

Ex: 2 Problem 4.825



$$R_i = R_f = 10 \text{ K}\Omega$$

$$R_L = 500 \Omega$$

$$C_f = 1 \text{ MF}$$

$$C_L = 10 \mu\text{F}$$

Req's

a) differential eqn.

b) static gain.

c) natural frequency.

d) damping Factor.

" Solution "

at node (1):

KCL

$$i_1 + i_2 = 0$$

$$\frac{V_i - V_1}{R} + \frac{V_2 - V_1}{R} = 0$$

Op-amp
eqn

$$V_1 = V_+ = 0$$



$$V_i = -V_2 \rightarrow (1)$$

at node (2):

KCL

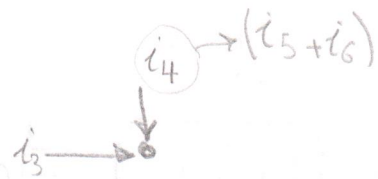
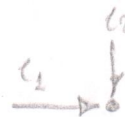
$$i_3 + i_4 = 0$$

$$i_3 + i_5 + i_6 = 0$$

$$\frac{V_2 - V_3}{R_i} + \frac{V_4 - V_3}{R_f} + C \frac{d}{dt} (V_4 - V_3) = 0$$

Op-amp
eqn

$$V_3 = V_+ = 0$$



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$$\frac{V_2}{R_i} + \frac{V_4}{R_f} + C_f V_4' = 0 \rightarrow (2)$$

$$C_f V_4' + \frac{V_4}{R_f} = \frac{V_i}{R_i} \rightarrow (3) \Rightarrow \left(C_f D + \frac{1}{R_f} \right) V_4 = \frac{V_i}{R_i}$$

at node (3) KCL

$$i_7 + i_8 = 0$$

$$\frac{V_4 - V_o}{R_L} + C_L \frac{d}{dt} (0 - V_o) = 0$$

$$C_L V_o' + \frac{V_o}{R_L} = \frac{V_4}{R_L} \rightarrow (4)$$

$$\cancel{C_L V_o' + \frac{V_o}{R_L} = \frac{1}{R_L} \left[\frac{V_i}{R_i \left[C_f D + \frac{1}{R_f} \right]} \right]}$$

↓ diff w.r.t time & $\times R_L$

$$\left. \begin{aligned} V_4 &= R_L C_L V_o' + V_o \rightarrow (5) \\ V_4' &= R_L C_L V_o'' + V_o' \rightarrow (6) \end{aligned} \right\} \text{sub in eqn (3)}$$

$$C_f [R_L C_L V_o'' + V_o'] + \frac{R_L C_L V_o' + V_o}{R_f} = \frac{V_i}{R_i} \rightarrow \times R_f$$

$$R_f C_f C_L R_L V_o'' + (R_f C_f + R_L C_L) V_o' + V_o = \frac{R_f}{R_i} V_i \rightarrow \text{Req (a)}$$

$$m x'' + b x' + k x = F(t)$$

Gr static gain

يعني في حالة عدم الحركة تكون $0 = x''(x')$

$$G = \left(\frac{V_o}{V_i} \right)_{V_o' = V_o'' = 0} = \frac{R_f}{R_i} = \frac{10}{10} = 1$$

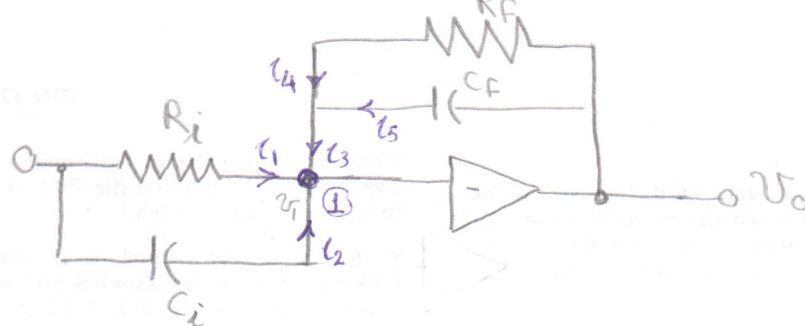
$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{1}{R_f C_f R_L C_L}} = 141.42 \text{ rad/sec}$$

$$\zeta = \text{damping factor} = \frac{b}{b_c} = \frac{R_f C_f + R_L C_L}{2 \times R_f R_L C_f C_L \times \omega_n} = 1.06$$

$(2m\omega_n)$ x'' جولو $2 \times \omega_n$

Ex 3

Prob/4-27



Req's a) diff. eqn

b) Transfer Function $\frac{V_i(s)}{V_o(s)}$

" Solution "

at node (1) KCL

$$i_1 + i_2 + i_3 = 0$$

$$i_3 = i_4 + i_5$$

$$\therefore i_1 + i_2 + i_4 + i_5 = 0$$

$$\frac{V_i - V_1}{R_i} + C_i \frac{d}{dt} (V_i - V_1) + \frac{(V_o - V_1)}{R_f} + C_f \frac{d}{dt} (V_o - V_1) = 0$$

$$\boxed{V_+ = V_1 = 0} \rightarrow \text{OP-amp eqn}$$

$$\frac{V_o}{R_f} + C_f \dot{V}_o = - \left[\frac{V_i}{R_i} + C_i \dot{V}_i \right]$$

$$\boxed{R_f C_f \dot{V}_o + V_o = - \frac{R_f}{R_i} [R_i C_i \dot{V}_i + V_i]} \rightarrow \text{(a)}$$

Take {L.T}

$$(R_f C_f s + 1) V_o(s) = - \frac{R_f}{R_i} [R_i C_i s + 1] V_i(s)$$

$$\frac{V_i(s)}{V_o(s)} = - \frac{R_f C_f s + 1}{\frac{R_f}{R_i} [R_i C_i s + 1]}$$

Electromechanical systems

DC. motors are essential in control system Two Types of D.C motors

1] Armature - Controlled DC motors (more Popular).

2] Field Controlled DC motors.

* Elemental Relations of Electromechanical systems:

The mechanical motion of the rotor relative to the stator affects the electromotive force (emf) voltage developed within the motor:

There are two critical relations for el-me systems.

① The back emf voltage E_b across a DC motor is proportional to the angular speed of the motor rotor.

$$E_b = K_e \omega = K_e \theta^\circ$$

② The Torque developed by the motor is proportional to the current.

$$T = K_t \cdot I_a$$

where

E_b = back emf voltage

θ = angular displacement of rotor ($\theta^\circ = \omega$)

T = torque applied to the rotor (developed by motor)

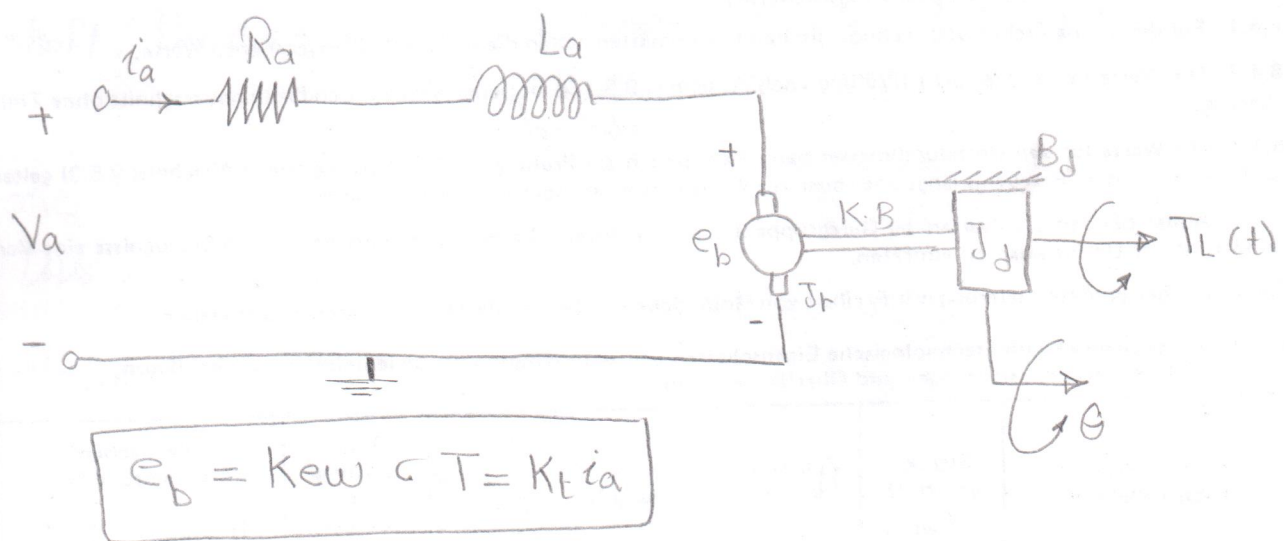
K_e = emf constant of the motor $V/K.r.p.m$

K_t = torque constant of the motor $\frac{in \cdot ozf}{A}$

K_e & K_t are the same [Listed in the specifications sheet of motor]

They have the same numerical value if expressed in [MKs] or [CGS]

I Armature - Controlled DC motors



The shaft is assumed mass less

B = Coef. of torsional viscous damping of the shaft

K = torsional stiffness of the shaft

B_d = Coef. of viscous damp associated with the disk

i_f = Field Current \rightarrow Stator

J_d = mass moment of inertia of the disk $\text{Kg} \cdot \text{m}^2$

J_r = mass moment of inertia of the rotor

i_a = armature current

L_a = " inductance

R_a = " Resistance

V_a = " voltage [V]

a) A simple model "Rigid shaft"

The shaft, the rotor and the disk lumped as a single rigid body

$$J = J_r + J_d$$

1/p one V_a

o/p two i_a and θ

* for electrical circuit

$$\text{KVL} \quad \sum V_{\text{drop}} = 0 \cdot 0$$

$$V_{ra} + V_{La} + E_b - V_a = 0$$

$$R_a i_a + L_a \frac{di_a}{dt} + K_e \theta = V_a$$

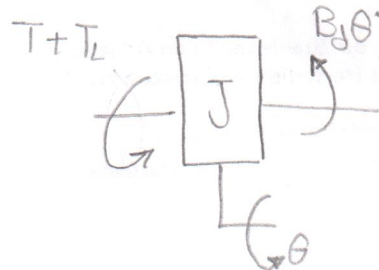
$$L_a i_a + R_a i_a + K_e \theta = V_a \rightarrow (1)$$

* for mechanical Part

$$\sum M = J \ddot{\theta}$$

$$T + T_L - B_d \dot{\theta} = J \ddot{\theta}$$

$$J \ddot{\theta} + B_d \dot{\theta} - K_t i_a = T_L(t) \rightarrow (2)$$



$$J \ddot{\theta} + B_d \dot{\theta} - K_t i_a = T_L \rightarrow (2)$$

$$L_a i_a + R_a i_a + K_e \theta = V_a \rightarrow (1)$$

Take (2, 1)

$$(Js + B_d)W(s) - K_t I_a(s) = T_L(s) \rightarrow (3)$$

$$(L_a s + R_a) I_a(s) + K_e W(s) = V_a(s) \rightarrow (4)$$

$$W(s) = \frac{\begin{vmatrix} T_L(s) & -K_t \\ V_a(s) & L_a s + R_a \end{vmatrix}}{\begin{vmatrix} Js + B_d & -K_t \\ K_e & L_a s + R_a \end{vmatrix}}$$

$$I_a(s) = \frac{\begin{vmatrix} Js + B_d & T_L(s) \\ K_e & V_a(s) \end{vmatrix}}{\begin{vmatrix} Js + B_d & -K_t \\ K_e & L_a s + R_a \end{vmatrix}}$$

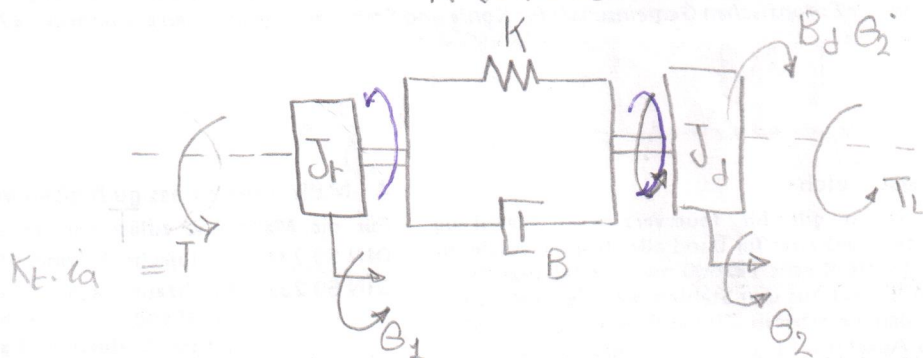
$$\Delta(s) = \begin{vmatrix} Js + B_d & -K_t \\ K_e & L_a s + R_a \end{vmatrix}$$

$$\Delta(s) = \left(s^2 + \frac{B_d L_a + J R_a}{J L_a} s + \frac{B_d R_a + K_e K_t}{J L_a} \right) \cdot J L_a$$

Kramer method

$$W(s) = \frac{T_L(s)(L_a s + R_a) + K_t V_a(s)}{\Delta s}$$

B) A more complex model "flexible damped shaft"



* For electrical circuit: (KVL) $\square V_{drop} = 0.0$

$$L_a \dot{i}_a + R_a i_a + K_e \theta_1 = V_a \rightarrow (1)$$

* For mechanical Part:

Rotor $J_r \ddot{\theta}_1 = -B(\dot{\theta}_1 - \dot{\theta}_2) - K(\theta_1 - \theta_2) + K_t i_a$

$$J_r \ddot{\theta}_1 + B \dot{\theta}_1 - B \dot{\theta}_2 + K \theta_1 - K \theta_2 = K_t i_a \rightarrow (2)$$

Disk $J_d \ddot{\theta}_2 = B(\dot{\theta}_1 - \dot{\theta}_2) + K(\theta_1 - \theta_2) + T_L - B_d \dot{\theta}_2$

$$J_d \ddot{\theta}_2 + (B + B_d) \dot{\theta}_2 - B \dot{\theta}_1 + K \theta_2 - K \theta_1 = T_L \rightarrow (3)$$